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Risk-quantification of Complex Systems by Matrix-based System Reliability Method





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System risk estimates for decision-making



Contents

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 - Post-earthquake connectivity of a transportation network
 - Seismic damage of a bridge structure system
 - Progressive failure of a truss structure

Challenges in system reliability

- Complexity of system event description
 - Difficult to identify cut sets or link sets
 - Boolean description ~ lengthy; inconvenient to handle
 - Makes system reliability *analysis* complex as well
- Statistical dependence between components
 - "Environment dependence" or "common source effects"
 - Expensive or infeasible to provide complete information on dependence ~ theoretical bounding formulas
- Incomplete information
 - Not very flexible in incorporating various information
- Statistical inference for decision-making

Existing system reliability methods

Theoretical bounding formulas (Ditlevsen 1979)

$$P_{1} + \sum_{i=2}^{n} \max\left(P_{i} - \sum_{j=1}^{i-1} P_{ij}, 0\right) \le P\left(\bigcup_{k=1}^{n} E_{k}\right) \le P_{1} + \sum_{i=2}^{n} \left(P_{i} - \max_{j \le i} P_{ij}\right)$$

• FORM approximation (Hohenbichler and Rackwitz 1983)

$$P(E_{series}) = 1 - \Phi(\beta, \mathbf{R}) \quad P(E_{parallel}) = \Phi(-\beta, \mathbf{R})$$

Monte Carlo simulations

$$P(E_{\text{system}}) = \int_D f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} \cong \frac{\#(\mathbf{x} \in D)}{\#(\mathbf{x})}$$

LP bounds method (Song and Der Kiureghian 2003)
 → generalized to a Matrix-based System Reliability (MSR) method

Matrix-based Formulation

Matrix-based formulation of system failure:

$$P(E_{sys}) = \mathbf{c}^{\mathrm{T}}\mathbf{p}$$

* Example:
$$P(E_1E_2 \cup E_3) = p_1 + p_2 + p_3 + p_4 + p_5$$

= $\begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 0 & 0 & 0 \end{bmatrix}$.
 $\begin{bmatrix} p_1 & p_2 & p_3 & p_4 & p_5 & p_6 & p_7 & p_8 \end{bmatrix}^{\mathrm{T}}$



- c: "event" vector
 - \sim describes the system event of interest

p: "probability" vector

~ likelihood of component joint failures

Identification of event vector, c

Matrix-based event operations:

$$\mathbf{c}^{\overline{E}} = \mathbf{1} - \mathbf{c}^{E}$$

$$\mathbf{c}^{E_{1} \cdots E_{n}} = \mathbf{c}^{E_{1}} \cdot \mathbf{c}^{E_{2}} \cdot \mathbf{c}^{E_{n}}$$

$$\mathbf{c}^{E_{1} \cup \cdots \cup E_{n}} = \mathbf{1} - (\mathbf{1} - \mathbf{c}^{E_{1}}) \cdot \mathbf{c}^{E_{2}} \cdot \mathbf{c}^{E_{2}} \cdot \mathbf{c}^{E_{n}}$$

- Efficient and easy to implement by matrix-based computing languages, e.g. Matlab®, Octave
- Can construct directly from event vectors of components and other system events
- Can develop/use problem-specific algorithms to identify event vectors

Computation of probability vector, p

 Iterative matrix-based procedure for statistically independent (s.i.) components



Statistical dependence b/w components

By total probability theorem,

$$P(E_{sys}) = \int_{\mathbf{x}} P(E_{sys} | \mathbf{x}) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}$$
$$= \int_{\mathbf{x}} \mathbf{c}^{\mathrm{T}} \mathbf{p}(\mathbf{x}) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}$$
$$= \mathbf{c}^{\mathrm{T}} \widetilde{\mathbf{p}}$$

- Utilize conditional s.i. of components given an outcome of random variables X causing component dependence e.g. Earthquake magnitude for a bridge system
- Event vector c is independent of this consideration ~ no need to construct the probability vector for new system events

"What if not explicitly identified?"

 Example: approximation by Dunnett-Sobel (DS) correlation matrix (1955)

$$Z_i \sim N(\mathbf{0}, \mathbf{R}), \ \rho_{ij} = r_i \cdot r_j$$
$$Z_i = \sqrt{1 - r_i^2} U_i + r_i X,$$

- Z_i , i=1,...,n are conditional s.i. given X=x
- Fit the given correlation matrix with a DS correlation matrix with the least square error
- Can generalize it further for better approximations

$$Z_i \sim N(\mathbf{0}, \mathbf{R}), \rho_{ij} = a_i a_j + b_i b_j$$
$$Z_i = \sqrt{1 - a_i^2 - b_i^2} U_i + a_i X + b_i Y$$

Incomplete information

• LP bounds method (Song and Der Kiureghian 2003)

minimize(maximize) $\mathbf{c}^{\mathrm{T}}\mathbf{p}$ subject to $\mathbf{A}_{1}\mathbf{p} = \mathbf{b}_{1}$ $\mathbf{A}_{2}\mathbf{p} \ge \mathbf{b}_{2}$ $\mathbf{A}_{3}\mathbf{p} \le \mathbf{b}_{3}$

- A₁, A₂, A₃: event vectors for which probabilities or bounds are available
- **b**₁, **b**₂, **b**₃: available probabilities or bounds
- Has been successfully applied to various systems (Song and Der Kiureghian 2003a, 2003b, 2006)

Conditional prob./importance measure

Conditional probability Importance Measure (CIM)

$$CIM_{i} = P(E_{i} | E_{sys}) = \frac{P(E_{i}E_{sys})}{P(E_{sys})}$$

Fussell-Vesely IM

$$FV_i = \frac{P(\bigcup_{k:C_k \supseteq E_i} C_k)}{P(E_{sys})}$$

•
$$P(E_{sys}')/P(E_{sys}) = (\mathbf{c}'^{\mathsf{T}}\mathbf{p}) / (\mathbf{c}^{\mathsf{T}}\mathbf{p})$$

 Once the system reliability is done, only additional task is to find the event vector for a new system event

Kang, Song and Gardoni (2007)

ICASP10 (July); Reliability Engineering and System Safety (under review)



- Post-earthquake disconnection from the critical facility
- Fragilities for bridges (Gardoni et al. 2003)
- Deterministic attenuation relationship used
- For given magnitude, the bridge component failures are conditional s.i.



Conditional probability of disconnection of cities

Probability of disconnection of cities



Conditional probability of disconnection of counties

Prob (No. of failed bridges $\geq k$)





$$P(E_i | E_{sys}) = \frac{P(E_i E_{sys})}{P(E_{sys})} = \frac{\mathbf{c}^{\mathsf{T}} \mathbf{\tilde{p}}}{\mathbf{c}^{\mathsf{T}} \mathbf{\tilde{p}}}$$

Importance measure of components w.r.t. the likelihood of at least a disconnection

Appl. II: Damage of a bridge structural system

Song and Kang (2007) ~ ASCE EMD conference (June)



- Nielson (2005) developed analytical fragilities of bridge components such as bearings, abutments and columns
- Identified the statistical dependence between demands
- Probability that at least one component fails (series system)
- Performed MCS to account for component dependence

Appl. II: Damage of a bridge structural system

* Safety Factor $F_i = \ln C_i - \ln D_i$

* Fragility $P(LS_i \mid IM) = P(F_i \le 0 \mid IM)$ $= P\left(Z_i \le -\frac{\mu_{F_i}}{\sigma_{F_i}} \mid IM\right)$ $= \Phi\left[-\frac{\mu_{F_i}(IM)}{\sigma_{F_i}(IM)}\right]$ * Correlation $Q_i = Q_i$

Correlation
$$\rho_{Z_i Z_j} = \rho_{F_i, F_j} = \frac{(\zeta_{D_i} \cdot \zeta_{D_j})}{(\zeta_{C_i}^2 + \zeta_{D_i}^2)^{1/2} (\zeta_{C_j}^2 + \zeta_{D_j}^2)^{1/2}} \cdot \frac{\rho_{\ln D_i, \ln D_j}}{(\rho_{\ln D_i, \ln D_j})}$$

* Fitting by DS-class corr. matrix: average of percentage error ~ 3%

Appl. II: Damage of a bridge structural system



System fragility (at least one)

Appl. III: Progressive failure of a truss structure

Song and Kang (2007) ~ ASCE EMD conference (June)



 $P(\overline{E}_{sys}) = P[\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6} \cup (E_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6})(\overline{E}_{7}\overline{E}_{8}\overline{E}_{9}\overline{E}_{10}\overline{E}_{11})$ $\cup (\overline{E}_{1}E_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6})(\overline{E}_{12}\overline{E}_{13}\overline{E}_{14}\overline{E}_{15}\overline{E}_{16}) \cup \cdots$ $\cup (\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}E_{6})(\overline{E}_{32}\overline{E}_{33}\overline{E}_{34}\overline{E}_{35}\overline{E}_{36})]$

Appl. III: Progressive failure of a truss structure

 $P(\overline{E}_{sys}) = P[\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6} \cup (E_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6})(\overline{E}_{7}\overline{E}_{8}\overline{E}_{9}\overline{E}_{10}\overline{E}_{11})$ $\cup (\overline{E}_{1}E_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6})(\overline{E}_{12}\overline{E}_{13}\overline{E}_{14}\overline{E}_{15}\overline{E}_{16}) \cup \cdots$ $\cup (\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}E_{6})(\overline{E}_{32}\overline{E}_{33}\overline{E}_{34}\overline{E}_{35}\overline{E}_{36})]$

Disjoint link sets (36→11)

 $P(\overline{E}_{sys}) = P(\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6}) + P(E_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}\overline{E}_{6}\overline{E}_{7}\overline{E}_{8}\overline{E}_{9}\overline{E}_{10}\overline{E}_{11})$ $\cdots + P(\overline{E}_{1}\overline{E}_{2}\overline{E}_{3}\overline{E}_{4}\overline{E}_{5}E_{6}\overline{E}_{32}\overline{E}_{33}\overline{E}_{34}\overline{E}_{35}\overline{E}_{36})$

> Perfect correlation 7 systems with 6 components

Appl. III: Progressive failure of a truss structure



- System collapse fragility curve given abnormal load
- Verified through MCS
- Importance of members (components)
- Sensitivity of fragility w.r.t. design parameters

